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Influence of Heat and Humidity

on the Bronchospastic Response to Exercise in Asthma

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Heat, humidity and Exercise-Induced Asthma

Results are reported of a study on

20. ABSTRACT *(Continue on reverse side if necessary and identify by block number)*

We examined the bronchospastic response of 8 asthmatics who exercised while breathing air under 4 conditions: (1) ambient room temperature and water content; (2) body temperature and ambient water content; (3) ambient room temperature fully saturated; and (4) body temperature fully saturated. These test conditions were performed in random order. Multiple aspects of pulmonary mechanics were measured before and 5 minutes after exercise. When air at ambient conditions was inhaled, the expected airway obstruction developed post-

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exercise and all variables changed significantly from their pre-challenge values. Heating the air to body temperature did not influence this response. Increasing the humidity at ambient temperatures significantly blunted the response and body temperature fully saturated air completely prevented from occurring. Thus, the water content of inspired air is an important variable in the development of exercise-induced asthma.

INTRODUCTION:

It is a well recognized clinical phenomenon that asthmatic individuals complain that exposure to various weather extremes, such as cold or high humidity, will often cause acute exacerbations of their disease. Although there is little objective evidence to support such associations, they are so ingrained that it is widely believed that living in a warm, dry climate will ameliorate the symptoms of this illness. In the course of investigating the effects of climatic conditions on airway reactivity in asthmatics, we have been able to demonstrate that, at least, part of these complaints have a basis in fact. When asthmatics were made to exercise while breathing subfreezing air, we found that their post-exertional bronchospastic response was markedly accentuated (1). Since air at sub-zero temperatures contains virtually no water, our findings raised the possibility that the synergism between exercise and cold air in asthmatics might be due to some sort of defect which interferes with their ability to completely heat and humidify air during inspiration. If this were so, then preconditioning of the inspirate during exercise might possibly modify the magnitude of the subsequent airway obstruction and thereby give some insights into the mechanisms underlying exercise-induced asthma. Our results form the basis of this report.

ABSTRACT

We examined the bronchospastic response of 8 asthmatics who exercised while breathing air under 4 conditions: (1) ambient room temperature and water content; (2) body temperature and ambient water content; (3) ambient room temperature fully saturated; and (4) body temperature fully saturated. These test conditions were performed in random order. Multiple aspects of pulmonary mechanics were measured before and 5 minutes after exercise. When air at ambient conditions was inhaled, the expected airway obstruction developed post-exercise and all variables changed significantly from their pre-challenge values. Heating the air to body temperature did not influence this response. Increasing the humidity at ambient temperatures significantly blunted the response and body temperature fully saturated air completely prevented it from occurring. Thus, the water content of inspired air is an important variable in the development of exercise-induced asthma.

METHODS

Eight atopic individuals, 1 man and 7 women, with reproducible exercise-induced asthma previously documented in our laboratory, served as subjects for this investigation. Their mean age was 22.9±2.0 (SD) years, and all met the American Thoracic Society's definition of asthma (2). All refrained from taking any medication for at least 12 hours prior to any study day. None had used gluco-corticoids or cromolyn sodium for at least a month before these studies. Informed consent was obtained from each participant.

We measured airway resistance and total lung capacity with its subdivisions in a variable pressure plethysmograph that was serially interfaced to an analog recorder (Electronics for Medicine, White Plains, New York), and a minicomputer (Lab 8E, Digital Equipment Corporation, Maynard, Mass.) (3,4). Resistance was converted to its reciprocal, conductance, and expressed as a conductance volume ratio termed specific conductance (SG_{AW}) (5). Four to five measurements of each variable were obtained and the mean computed. These data were considered acceptable if their coefficients of variation were five percent or less. Maximum forced exhalations were then performed in triplicate using a waterless spirometer (Electro Med Model 780, Houston, Texas). One-second forced expiratory volumes (FEV_1) and maximum mid-expiratory flow rates (MMF) were computed by standard techniques. The best effort, as defined by the curve with the largest forced vital capacity and FEV_1, was used for analysis.

Inspired air was conditioned by having the subjects breathe through a heat exchanger which was kept either at ambient room or body temperatures. The exchanger consisted of a heavily insulated, 76 cm long copper tube with an internal diameter of 6.5 cm, equipped with a 10.7 cm (ID) one-way valve on the inspiratory port. In the body temperature experiments, water maintained at 37°C in a bath was circulated by pump through copper coils around the walls of

the exchanger. Inspired air temperatures in all experiments were continuously recorded by a thermocouple situated in the airstream within the exchanger and located 10 cm upstream from the mouth. Expired gas was directed away from the exchanger through another one-way valve into a Tissot spirometer so that tidal volume (V_T), respiratory frequency (f), and minute ventilation ($\dot{V}_E$) could be continuously recorded. Heart rate was also monitored continuously.

The water content of the inspired air was brought to full saturation by forcing room air, with the aid of a blower, into a copper manifold (3.5 cm ID) that was perforated with multiple small holes, and was immersed in a separate water bath maintained at 50 or 29°C for the body and room temperature experiments, respectively. The incoming air then bubbled through the water where it was heated and fully humidified. It was then collected in a 25 L meteorological balloon which was in series with the one-way valve on the inspiratory port of the exchanger. While in the balloon, the air was permitted to cool to either 41 or 27°C depending upon the experiment, so as to permit excess moisture to "rain out". As the air entered the exchanger, it then cooled further to either room or body temperature as determined by the exchanger settings, but it maintained its saturation of 100%. Adjusting the blower speed and the amount of filling of the balloon allowed us to control the rate of cooling and still provide sufficient conditioned air to meet the ventilatory demands of the exercising subjects. A thermocouple measured the temperature of the air leaving the balloon. During experiments that employed ambient room humidity, the bubble humidifier was disconnected from the exchanger.

The water content of the air leaving the mouthpiece of the exchanger was verified by sampling the airstream during simulated ventilations of up to 150 L/min at both body and ambient temperatures. Water content of the air was determined by drawing a known volume of air through glass drying tubes containing

anhydrous calcium sulfate (W.A. Hammond Drierite Co., Xenia, Ohio). From the change in weight of the drying tube and the volume of air sampled, water content was expressed as mg H_2O/L air. The ambient temperature and humidity of the room were measured with a standard mercury thermometer and a hygroscopic membrane hygrometer (Bacharach Instrument Co., Pittsburgh, Penna.), respectively. The accuracy of the latter was also verified by sampling room air and determining its water content by standard physical means as above.

In the first series of experiments we investigated the effects of breathing air at body temperature with various humidities on the pulmonary mechanical response to exercise. This was accomplished by having the subjects perform three bouts of exhausting leg work on a cycle ergometer while breathing air at ambient temperature and water content, body temperature and ambient water content, or body temperature fully saturated, in a random fashion. The ambient condition experiment was used as a control. Each type of air was breathed for four minutes before, during, and for four minutes after exercise.

Upon completion of each exercise period, the subjects were allowed to rest for at least 1.5 hours while their pulmonary function returned to pre-exercise levels. When this occurred the exercise was then repeated using identical work loads, RPM, and durations for each individual. The mean workload was 806±178 (S.D.) kpm, and the mean duration of exercise was 3.13±0.54 (S.D.) minutes.

Exhausting leg work was used as the provocational stimulus because it was technically easier to have the subjects breathe through the exchanger from a fixed seated position. Previous experience with this form of maximum work had demonstrated that it is a highly effective and reproducible means of inducing bronchospasm (1,6,7). Similarly, the duration of work, the interval between studies, and the number of studies that could be performed within a day had all been previously verified as being appropriate (1,6-9).

Pulmonary mechanics were measured before and 5 minutes after cessation of work. Again, prior experiments demonstrated that this time sequence would coincide with the optimum response (1,6-9). As indicated, ventilations and heart rates were measured continuously before and during exercise. The data from the last minute of the rest and exercise periods were analyzed.

In order to isolate the effects of humidity per se, a second set of experiments were performed on a different day. In this study, air of ambient temperature was completely humidified, and the response compared to that seen with ambient temperature and water content. As before, the experimental sequence was randomized. The work loads were identical to those used on the first day and were kept constant for each study for each subject. Pulmonary mechanics, ventilation, and heart rates were measured as previously described.

The data were analyzed by paired t tests, and both one-and-two-factor analysis of variance.

RESULTS

These studies were performed in an airconditioned room at sea level where the ambient temperatures and relative humidities varied between 22 and 25°C and 23 and 53%, respectively. Since relative humidity is defined as the amount of water present in the air as a proportion of the quantity that the air can hold, and since the latter varies with temperature, a given water content can be associated with different relative humidities. For example, if the ambient water content were 10 mg H_2O/L air at a temperature of 25°C, this would correspond to a relative humidity of 43%. However, if this air were heated to 37°, relative humidity would fall to 23%, because the amount of water the air could contain at 37° has risen by 21 mg/L. Consequently, to avoid confusion, this report will present all saturation data in terms of absolute water content in mg of water per liter of air.

The validation data for the measurement of water content are contained in Figure 1. The data were obtained with the bubble humidifier at ventilations ranging from 80 to 150 L/min and at air temperatures of 24 and 37°C within the heat exchanger. The first panel demonstrates that there were no significant differences between the expected water contents and those physically measured, and the second shows that water content remained constant even at ventilations greatly in excess of those seen in this study.

The effects of exercise on pulmonary mechanics while breathing air at different temperatures and humidities are shown in Tables 1 through 4 and Figures 2 and 3. In the control experiment, the mean ambient temperature was 23.7±0.9°C (S.D.), and the water content ranged from 5.3 to 9.3 mg/liter of air (mean = 7.6± 1.6 mg H_2O/L air). During exercise, $\dot{V}_E$ was 71.3±9.0 L/min, and the mean heart rate was 165±11 beats/min. As can be seen in Table 1, significant airway obstruction developed. Specific conductance fell an average of 58% from its baseline valve, and FEV_1 and MMF decreased 24 and 20%, respectively, from theirs. Residual volume rose 61%. Heating the inspired air to 37.4±0.2°C, but leaving water content at ambient values (8.7±0.8 mg H_2O/L air), had no effect upon the response (Table 2, Figures 2 and 3). Comparisons of absolute values for the baseline and response data with those in the control experiment by a 2 factor analysis of variance did not reveal any differences in these two studies (F < 1.0 for every variable).

When the air was fully humidified (20.4±0.4 mg H_2O/L air) at ambient temperatures (22.9±0.14°C), airway obstruction still developed in that all variables changed significantly from control,(Table 3), but the magnitude of the response was significantly less than it was in the previous two experiments (p < 0.01 for each variable), (Figures 2 and 3). Specific conductance now fell only 23% while FEV_1 and MMF changed 9 and 18%, respectively. Residual volume was only 23% greater than its pre-exercise value. Having the subjects inspire air at body

temperature (37.1±0.5°C) with full saturation (44.1±1.0 mg H_2O/L air) abolished the response in that there was no significant decrement in lung function post-exercise (Table 4). In point of fact, the spirometric variables actually improved over pre-exercise values, MMF significantly so. Residual volume rose 16%, but these changes are no greater than those previously reported to occur in normal subjects following strenuous exertion (8,10). This response was significantly different from the previous 3 experiments at the 0.01 level or less for all aspects of mechanical lung function except RV. No differences were found between experiments 3 and 4 (ambient temperature fully saturated and body temperature fully saturated) for this index.

The trend in our data can be more clearly seen when the changes in each variable are pooled and plotted as a percent decrement from the control experimental response versus the inspired water content. As can be seen in Figure 4, when the water content doubled, the observed bronchospastic response halved. When it was again doubled to its maximum limit, obstruction did not develop.

It is unlikely that the differences in the magnitude of the response recorded above were due to variations in the application of the exercise stimulus. One factor analysis of variance demonstrates that there were no significant differences in either $\dot{V}_E$ or heart rates between any study ($\dot{V}_E$, F = 0.54; df = 3,31; p ns; HR, F = 0.30; df = 3,31; p ns).

DISCUSSION

The results of this study demonstrate that the magnitude of the bronchospastic response of asthmatics to exercise can be considerably blunted by increasing the water content of inspired air at ambient room temperatures and totally abolished by having the subjects inhale air at BTPS conditions. Although we have insufficient data to state categorically that these observations are causally related to the phenomenon of exercise-induced asthma, consideration of

the factors that determine the physiology of heat and water exchange in the air-
ways, in conjunction with the chronic mucosal changes seen in this illness (11,
12), suggest that our findings may explain part of the reaction sequence by which
physical exertion ultimately leads to airway obstruciton.

During inspiration, air is conditioned to have a temperature of 37°C and
44 mg of water/L by the time it reaches the alveoli. This is accomplished by
transferring sufficient quantities of heat and water from the respiratory mucosa
to correct for the differences in temperature and humidity between the ambient
air and that of the body per unit volume inhaled. Heating appears to occur
primarily by convection which is greatly facilitated by the turbulent flows
and large temperature gradients that are found in the upper air passages (13,14).
As the air is warmed, its capacity to hold water increases, and it is humidified
by the mucosa. The net effect of this heat and water exchange is to cool the
mucosa. During expiration the process reverses along thermal gradients by con-
vection and as the air temperature falls, its water capacity diminishes so con-
densation onto the mucosa ensues. This results in recovery by the mucosa of
between one third and one half of the heat transferred to the air during inspira-
tion. Of the two processes required to condition the inspirate -- i.e., direct
heating of the inspired air (0.304 Cal/L/°C) and the latent heat of vaporization
of water (0.58 Kcal/gm) -- the latter predominates, thus the vast majority of the
heat transferred by the mucosa is in the form of latent heat of vaporization.
Hence, it should be no surprise that in pre-conditioning the air, the effects of
humidity on the bronchospastic response predominated over temperature alone.

Matching inspired temperature to that of the body would be expected to
decrease the heat transfer across the mucosa only very little. By contrast,

increasing the water content of the inspirate, even at ambient temperatures, greatly decreases the heat transfer. Hence, the findings that humidity and not temperature influenced lung function are consistent with the idea that the quantity of heat transferred across the mucosal surface is a major determinant of the magnitude of the post-exercise bronchospastic response.

Why does bronchoconstriction develop under these circumstances in asthmatics and not in normal subjects? Theoretically, there are three possibilities. Because of the pathologic changes in their airways, asthmatics may not: (1) condition the inspired air normally; (2) recover as much heat and/or water on expiration as do normals; or (3) they may be unusually sensitive to effects of the physical stimulus of cooling. There are no data in the literatures to prove any of these points, but it is of interest that Caldwell et al. found the fraction of body heat dissipated by way of the respiratory tract to be higher in patients with lung disease than it is in normals (16). On the average, the ventilations in the present study were six times greater than in Caldwell's work, and it is to be expected that the heat loss was also commensurately greater.

Within the framework of the hypothesis that conditioning of inspired air may be defective in asthmatics, it seems pertinent to consider the differences in the response to ambient air exercise in two groups of subjects previously reported from this laboratory, since representatives of both groups are included in the present study (9). One group had a predominantly large airway response to exercise that was totally abolished by atropine, and the other had a predominantly small airway response which not affected by pretreatment with anticholinergics. It is tempting to speculate that in the first group, heat transfer and its effects were predominant in large airways where the density of irritant receptors is greatest (17). By contrast, it is possible that incompletely

conditioned air penetrated more deeply into the respiratory tract of the small airway group, and direct or local effects accounted in large part for the response.

It is not at all certain that these two groups are immutable. It is feasible that the severity of the illness prior to challenge dictated the location of the responses. For example, the patients with predominant small airway obstruction had more impaired lung function prior to challenge than did the large airway group. Consequently, in the former, it is reasonable to suggest that inflammatory process with the airways accounted for an insufficient conditioning of air until it reached more distal portions of the tracheobronchial tree. If this were true, then the site of obstruction induced by exercise would be expected to change as the patients underlying disease process improves. Firm conclusionsawait further experimentation, but preliminary observations suggest that when patients are repeatedly challenged over time with the same stimulus, the location of obstruction appears to change as the disease process waxes and wanes (E. R. McFadden, Jr. and R. H. Ingram, unpublished observations, 1977).

Since both populations had their responses blunted by cromolyn sodium, it appears likely that irrespective of site, mediatior release is involved in bringing about the bronchospasm, or that some other less specific effect of cromolyn was involved. The concept of mast cells being activated by non-immunologic stimuli in these circumstances is an intriguing one. It has been recently shown that there are histamine containing cells that are related to the mast cell-basophil series that can be readily lavaged from bronchial lumens of humans (18), and it is possible that they could be directly stimulated by the thermal conditions of their environment. Precedent for this reasoning can be derived from conditions like cold-induced urticaria and cholinergic urticaria in which

the chemical mediators of immediate hypersensitivity are released from mast cells within the skin in response to cold and heat, respectively, (19,20).

Irrespective of the ultimate path by which the obstruction develops, even if our findings are not causally related to the phenomenon of exercise-induced asthma, they clearly demonstrate that environmental conditions extraneous to the patient can profoundly influence the magnitude of the response. These conclusions are similar to those reached in a recent abstract (21). The clinical significance of these observations is that when one is attempting to determine such basic issues as reproducibility, prevalence, and effects of various thera-peutic maneuvers by performing exercise challenges spaced over days, variations or fluctuations in environmental temperature and humidity are significant inter-active variables that must be controlled. As our knowledge expands, it is expected that these climatic factors will be found to be unique to exercise because of the stress it puts upon the heat exchanging mechanisms of the respi-ratory tract and will play little or no role in other forms of bronchial challenges.

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LEGEND FOR FIGURES:

Figure 1. Validation experiments for the use of the Bubble Humidifier. The graph on the left plots the expected water content of the inspired air (derived from calculations using air temperature and relative humidity) on the horizontal axis versus measured contents at the mouthpiece of the exchanger with the humidifier in action on the vertical scale. The solid line is the line of identity. Each data point represents a separate determination. The zero point was obtained with compressed air. The graph on the right shows the stability of the inspired water content at various airflows through the humidifier-heat exchanger circuit. The data points represent the mean of several determinations.

Figure 2. Changes in specific conductance (SG_{AW}) and residual volume (RV) following exercise while inspiring air of various temperatures and water contents. The letters B and R below each graph represent baseline and response values, respectively. The data points are mean values, and the brackets represent one standard error.

Figure 3. Changes in one-second forced expiratory volumes (FEV_1) and maximum mid-expiratory flow rates (MMF) following exercise while inspiring air at various temperatures and water contents. The format is identical to Figure 2.

Figure 4. Comparison of the percentage decrement in response from the control observation as a function of increasing inspired water content. The data points represent the mean change seen when each index of pulmonary mechanics was pooled. The brackets represent one standard error of the mean.

Effects of Exercise on Pulmonary Mechanics While Breathing Air at Ambient Temperature and Humidity

Subject	T	WC	$\dot{V}_E$	HR	SG_{AW}		FEV_1		MMF		RV	
					B	R	B	R	B	R	B	R
1	23.5	6.7	62.2	160	0.14	0.04	2.22	1.84	1.09	0.92	2.06	2.77
2	25.0	5.3	55.4	146	0.16	0.08	2.65	2.42	1.87	1.49	1.08	1.26
3	25.0	5.3	71.2	174	0.12	0.04	2.55	2.07	1.89	1.09	1.32	1.71
4	23.0	8.8	75.4	158	0.11	0.06	3.13	2.02	2.45	1.15	1.91	3.82
5	23.0	9.0	75.7	164	0.13	0.07	2.69	2.31	1.78	1.35	1.74	2.46
6	24.0	9.3	78.7	176	0.14	0.05	2.72	1.39	2.41	0.66	1.01	2.98
7	23.0	7.6	82.8	162	0.13	0.06	2.98	2.01	2.27	1.22	1.76	2.23
8	23.0	8.6	69.2	180	0.09	0.04	1.74	1.50	2.01	0.91	1.12	2.19
Mean	23.7	7.6	71.3	165	0.13	0.06	2.59	1.95	1.83	1.09	1.50	2.43
S.D.	0.9	1.6	9.0	11	0.02	0.02	0.44	0.36	0.58	0.27	0.41	0.79
p	-	-	-	-	<0.001		<0.005		<0.01		<0.01	

$\dot{V}_E$ = minute ventilation in L/min; HR = heart rate in beats/min; T = temperature in °C; WC = water content in mg/L; SG_{AW} = specific conductance in L/sec/cm H_2O/L; FEV_1 = one-second forced expiratory volume in liters; MMF = maximum mid-expiratory flow rate in L/sec; RV = residual volume in liters. The p values refer to baseline-response comparisons.

Effects of Exercise on Pulmonary Mechanics While Breathing Air at Body Temperature and Ambient Water Content

Subject	T	WC	$\dot{V}_E$	HR	SG_{AW}		FEV_1		MMF		RV	
					B	R	B	R	B	R	B	R
1	37.0	6.9	65.3	152	0.15	0.04	2.40	1.12	1.37	0.46	1.60	3.21
2	37.5	9.2	67.2	142	0.14	0.06	2.29	1.73	1.37	0.89	1.09	1.74
3	37.5	9.2	76.1	168	0.11	0.04	2.68	1.60	2.06	0.73	1.49	2.47
4	37.0	8.6	93.4	168	0.11	0.07	3.73	2.96	3.00	2.18	1.69	2.83
5	37.5	9.2	67.5	164	0.12	0.09	2.51	2.30	1.63	1.45	1.66	2.00
6	37.5	8.8	70.6	166	0.13	0.04	2.82	1.56	2.46	0.94	1.53	3.15
7	37.5	9.0	81.7	162	0.12	0.06	2.75	2.68	2.05	1.75	1.77	2.04
8	37.5	8.8	60.4	174	0.08	0.04	1.75	1.51	0.88	0.79	1.18	1.98
Mean	37.4	8.7	72.7	162	0.12	0.06	2.62	1.93	1.85	1.15	1.50	2.43
S.D.	0.2	0.8	10.6	10	0.02	0.02	0.56	0.64	0.68	0.59	0.24	0.57
p	-	-	-	-	<0.001		<0.01		<0.01		<0.005	

$\dot{V}_E$ = minute ventilation in L/min; HR = heart rate in beats/min; T = temperature in °C; WC = water content in mg/L; SG_{AW} = specific conductance in L/sec/cm H_2O/L; FEV_1 = one-second forced expiratory volume in liters; MMF = maximum mid-expiratory flow rate in L/sec; RV = residual volume in liters. The p values refer to baseline-response comparisons.

Effects of Exercise on Pulmonary Mechanics While Breathing Air at Ambient Temperature Fully Saturated

Subject	T	WC	$\dot{V}_E$	HR	SG_{AW}		FEV_1		MMF		RV	
					B	R	B	R	B	R	B	R
1	23.0	20.5	56.3	168	0.14	0.08	2.36	2.03	1.28	0.95	-	-
2	23.0	20.5	71.0	144	0.11	0.11	2.16	2.00	1.23	1.16	1.06	1.23
3	22.0	19.5	76.4	168	0.12	0.08	2.73	2.63	2.47	2.11	1.49	1.82
4	23.0	20.5	83.9	164	0.10	0.09	3.90	3.46	3.34	2.45	1.31	1.99
5	23.0	20.5	76.4	156	0.17	0.15	2.77	2.50	2.18	1.50	1.38	1.45
6	23.0	20.5	71.8	148	0.16	0.11	3.16	2.93	2.94	2.99	1.06	1.37
7	23.0	20.5	71.5	164	0.10	0.06	2.67	2.44	2.00	1.57	1.92	2.34
8	23.0	20.5	60.3	172	0.14	0.10	2.30	2.17	1.80	1.49	0.92	1.02
Mean	22.9	20.4	71.0	161	0.13	0.10	2.76	2.52	2.16	1.78	1.31	1.60
S.D.	0.4	0.4	8.9	10	0.03	0.03	0.56	0.50	0.75	0.69	0.34	0.46
p	-	-	-	-	<0.005		<0.001		<0.01		<0.01	

$\dot{V}_E$ = minute ventilation in L/min; HR = heart rate in beats/min; T = temperature in °C; WC = water content in mg/L; SG_{AW} = specific conductance in $L/sec/cmH_2O/L$; FEV_1 = one-second forced expiratory volume in liters; MMF = maximum mid-expiratory flow rate in L/sec.; RV = residual volume in liters. The p values refer to baseline-response comparisons.

Effects of Exercise on Pulmonary Mechanics While Breathing Air at Body Temperature Fully Saturated

Subject	T	WC	$\dot{V}_E$	HR	SG_{AW}		FEV_1		MMF		RV	
					B	R	B	R	B	R	B	R
1	37.0	44	55.4	142	0.13	0.14	2.12	2.21	0.97	1.09	1.61	1.81
2	38.0	46	57.1	152	0.14	0.12	2.63	2.78	1.62	2.04	1.10	1.21
3	37.0	44	82.9	180	0.17	0.10	2.86	3.04	2.35	2.88	1.18	1.37
4	37.0	44	64.1	172	0.10	0.11	3.67	4.20	3.06	3.65	1.51	1.83
5	37.5	45	69.8	156	0.11	0.14	2.62	2.64	1.94	2.00	1.27	1.56
6	36.5	43	58.0	170	0.21	0.14	2.89	2.90	2.92	3.40	-	-
7	37.0	44	78.4	164	0.11	0.12	3.00	2.89	1.79	2.41	1.61	1.74
8	36.5	43	69.2	184	0.09	0.09	1.92	1.81	1.13	1.01	1.05	1.19
Mean	37.1	44.1	66.9	165	0.13	0.12	2.71	2.81	1.97	2.31	1.33	1.53
S.D.	0.5	1.0	10.1	14	0.04	0.02	0.54	0.70	0.76	0.98	0.24	0.28
p	-	-	-	-	NS		NS		<0.02		<0.001	

$\dot{V}_E$ = minute ventilation in L/min; HR = heart rate in beats/min; T = temperature in °C; WC = water content in mg/L; SG_{AW} = specific conductance in $L/sec/cmH_2O/L$; FEV_1 = one-second forced expiratory volume in liters; MMF = maximum mid-expiratory flow rate in L/sec; RV = residual volume in liters. The p values refer to baseline-response comparisons.
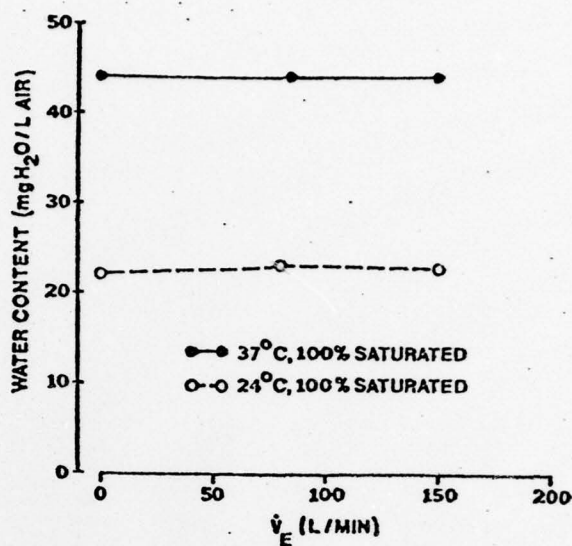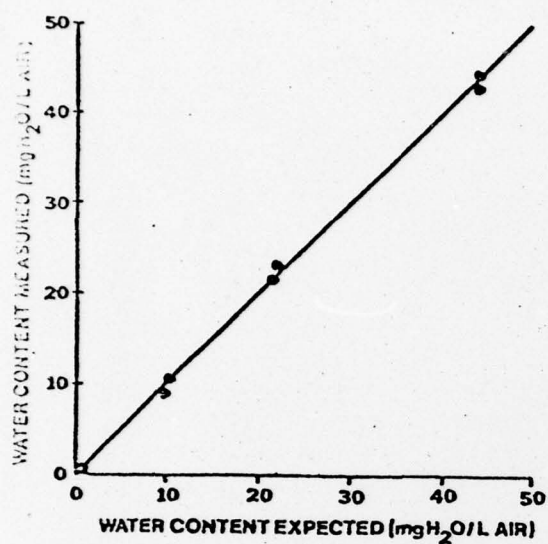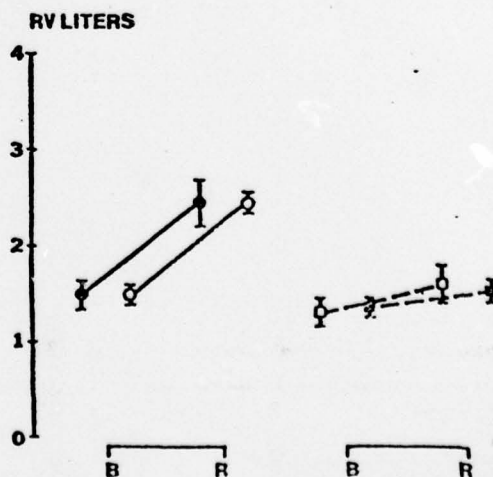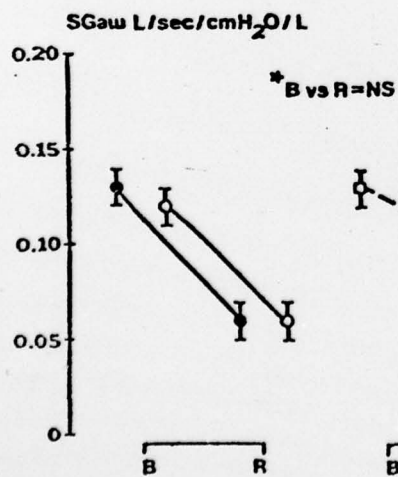
Fig 1

AMBIENT TEMP & WATER CONTENT
BODY TEMP AMBIENT WATER CONTENT
AMBIENT TEMP SATURATED
BODY TEMP SATURATED

FEV₁ LITERS

*B vs R = NS

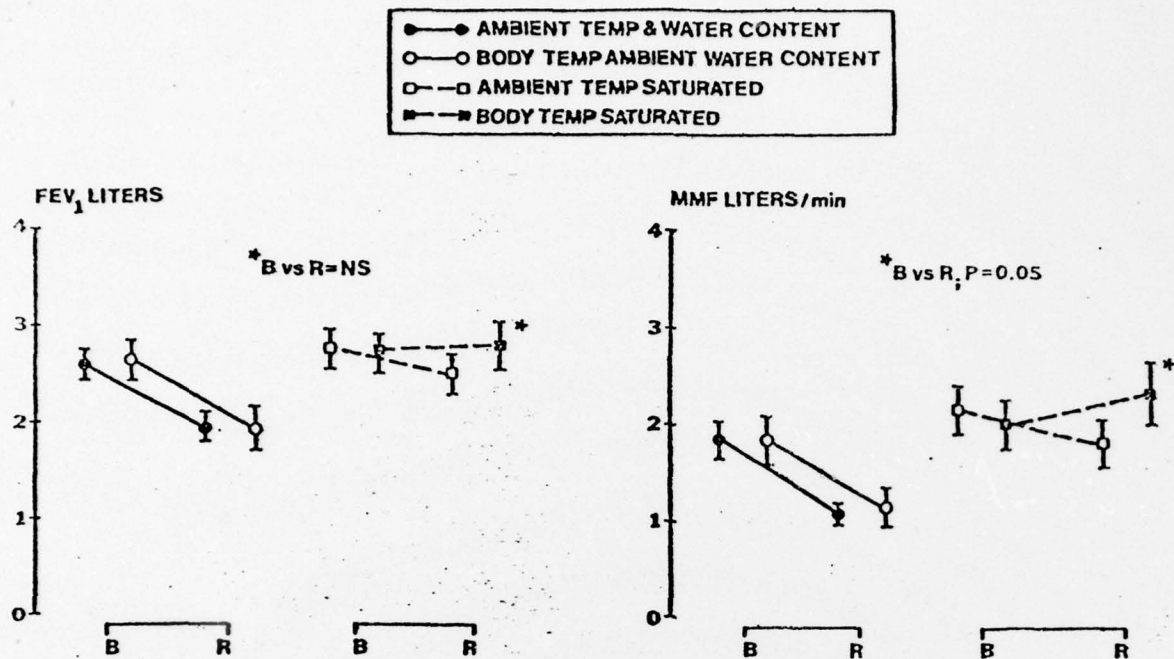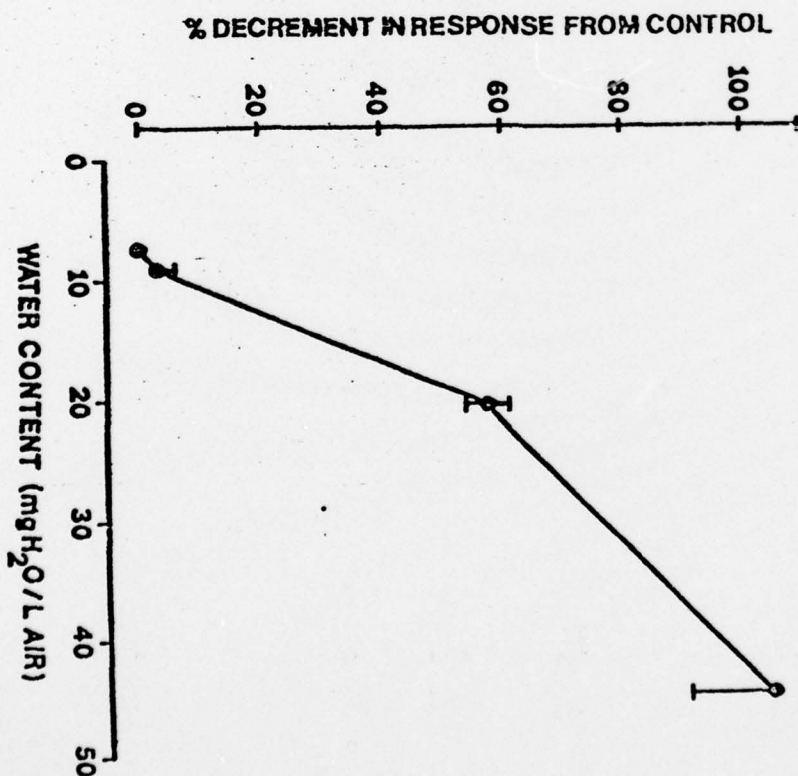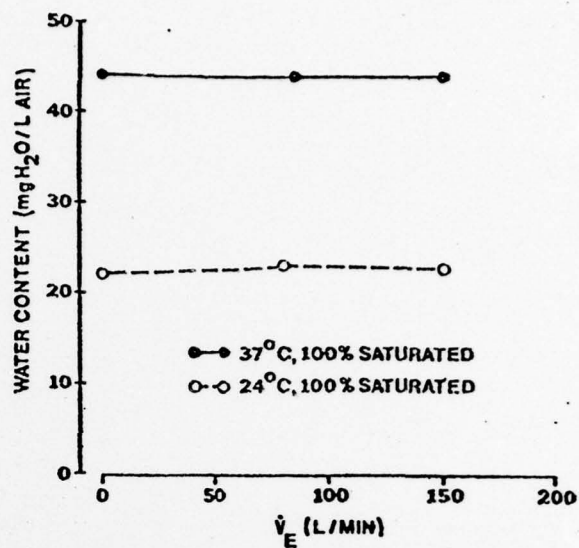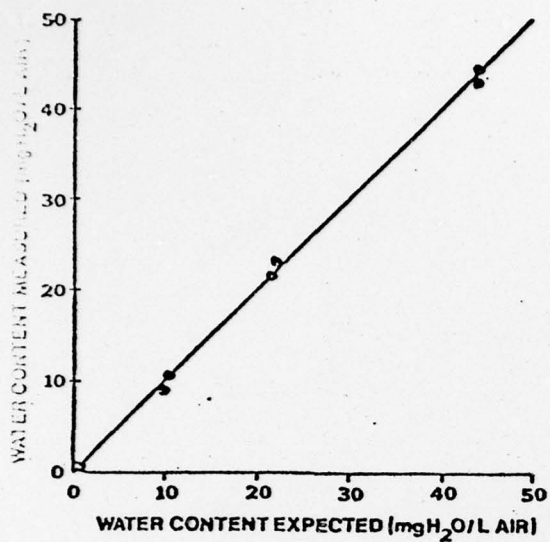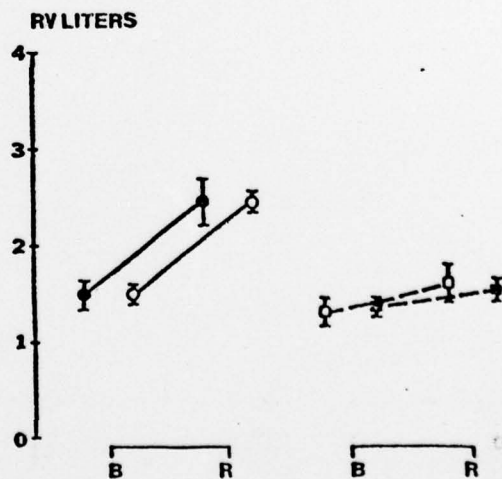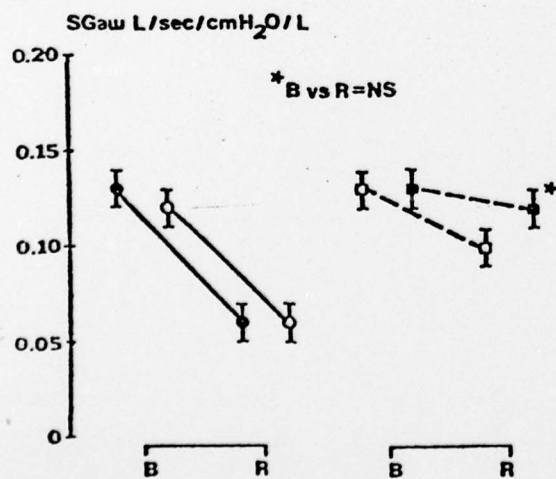MMF LITERS/min

*B vs R, P = 0.05

B   R   B   R

B   R   B   R

Fig 3

% DECREMENT IN RESPONSE FROM CONTROL

0   20   40   60   80   100

WATER CONTENT (mg H₂O / L AIR)

Fig 4

Upper left figure: Y-axis labeled "WATER CONTENT MEASURED (mgH₂O/L AIR)" with scale 0, 10, 20, 30, 40, 50. X-axis labeled "WATER CONTENT EXPECTED (mgH₂O/L AIR)" with scale 0, 10, 20, 30, 40, 50.

Upper right figure: Y-axis labeled "WATER CONTENT (mgH₂O/L AIR)" with scale 0, 10, 20, 30, 40, 50. X-axis labeled "V̇_E (L/MIN)" with scale 0, 50, 100, 150, 200. Legend:
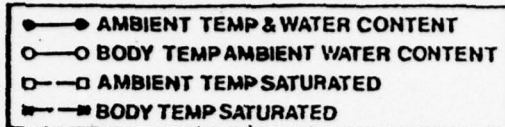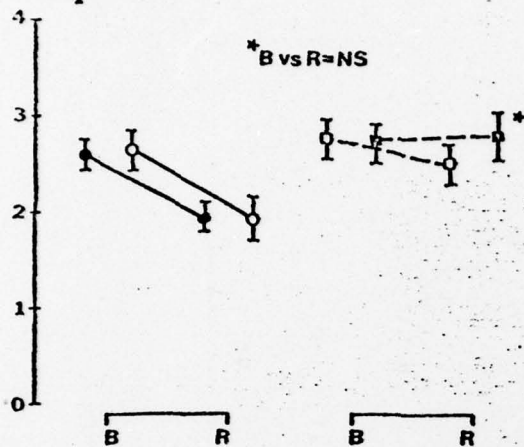● 37°C, 100% SATURATED
○ 24°C, 100% SATURATED

Legend box:
●——● AMBIENT TEMP & WATER CONTENT
○——○ BODY TEMP AMBIENT WATER CONTENT
□——□ AMBIENT TEMP SATURATED
■——■ BODY TEMP SATURATED

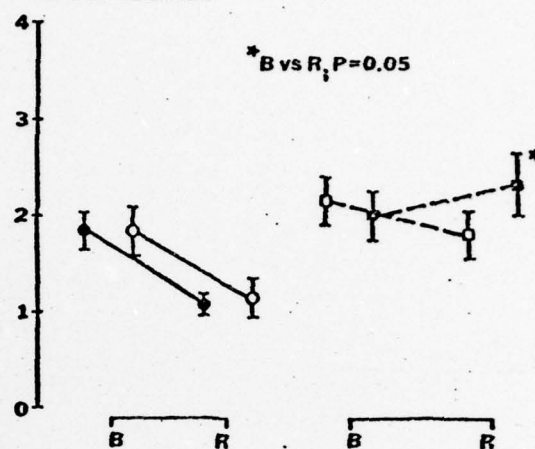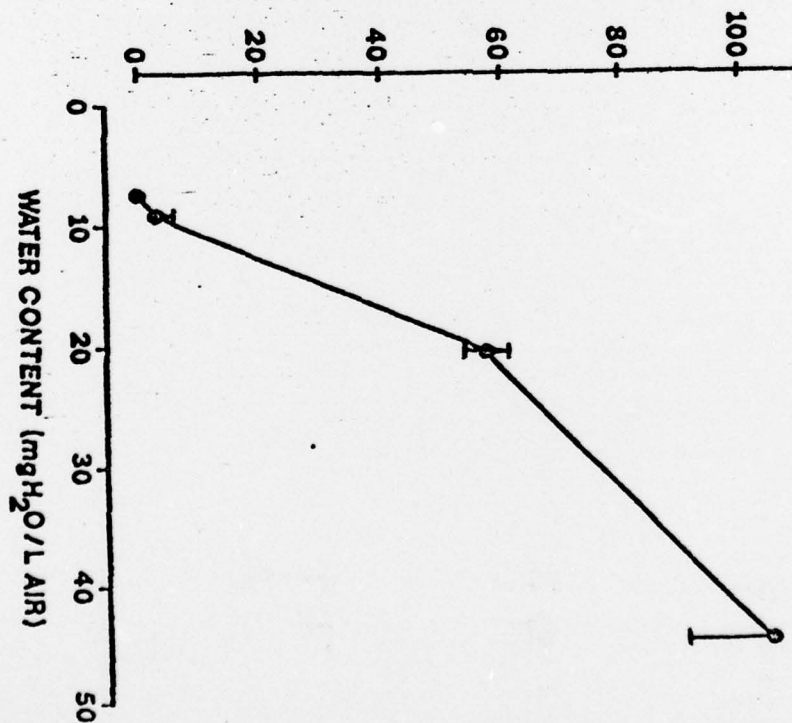Lower left figure: "SGaw L/sec/cmH₂O/L" Y-axis scale 0, 0.05, 0.10, 0.15, 0.20. "*B vs R=NS". X-axis labels B, R, B, R.

Lower right figure: "RV LITERS" Y-axis scale 0, 1, 2, 3, 4. X-axis labels B, R, B, R.

FEV$_1$ LITERS

*B vs R = NS

MMF LITERS/min

*B vs R, P = 0.05

4

3

2

1

0

B   R   B   R

B   R   B   R

% DECREMENT IN RESPONSE FROM CONTROL

0   20   40   60   80   100

0

10

20

30

40

50

WATER CONTENT (mg H$_2$O / L AIR)

a. The views of the author do not purport to reflect the positions of the Department of the Army or the Department of Defense.

b. Human subjects participated in these studies after giving their free and informed voluntary consent. Investigators adhered to AR 70-25 and USAMRDC Regulation 70-25 on Use of Volunteers in Research.